



SCHOOL OF ENERGY RESOURCES

**At the Forefront of Energy Innovation,
Discovery, and Collaboration**



Sealing Capacity Investigations of the Multiple Confining Layers at the RSU Geological CO₂ Storage Site



Z. Jiao, F. McLaughlin, S. Quillinan, Y. Ganshin, R. Bentley

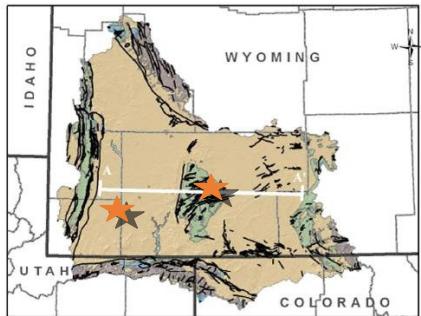
Carbon Management Institute
School of Energy Resources, University of Wyoming

Outline

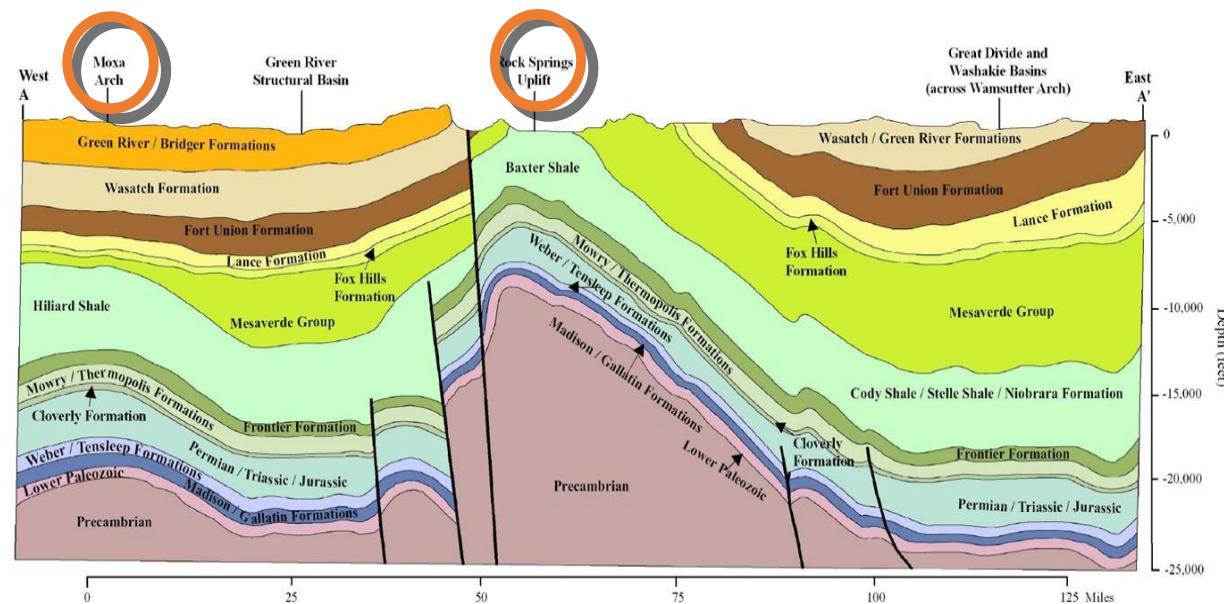
- 1. The Rock Springs Uplift (RSU) geological CO₂ storage site characterization**
- 2. The CO₂ storage capacity and CO₂ column height assessment of the RSU storage site**
- 3. Petrophysical and petrographic characteristics of confining layers at the RSU site**
- 4. Determination of the sealing capacities of the confining layers in a CO₂-brine-rock system**
- 5. Remarks**



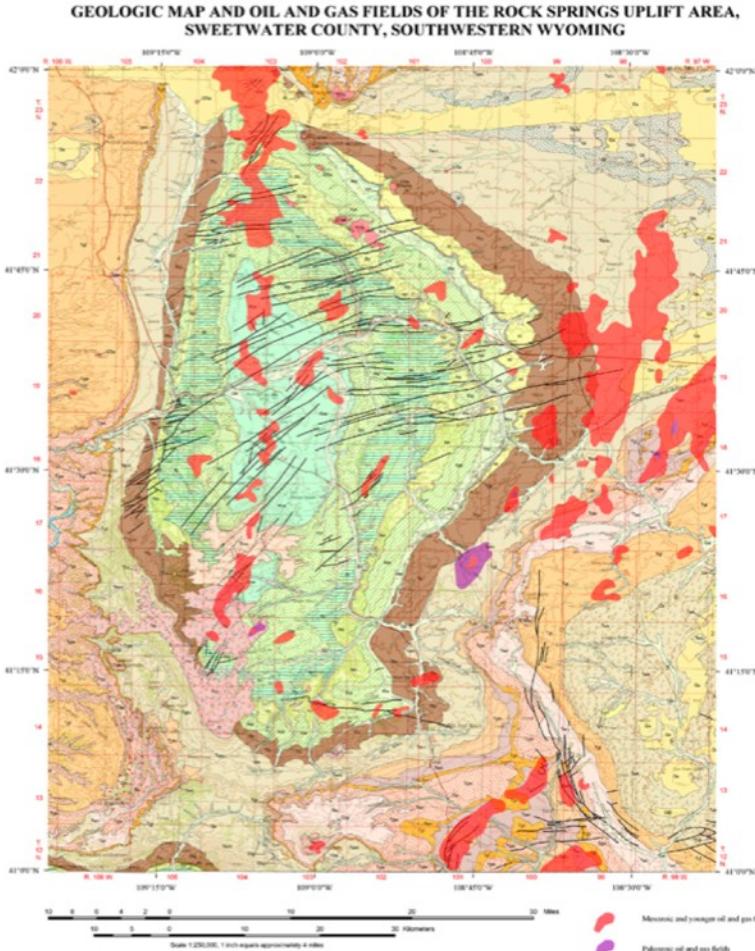
Priority Carbon Storage Sites in SW Wyoming



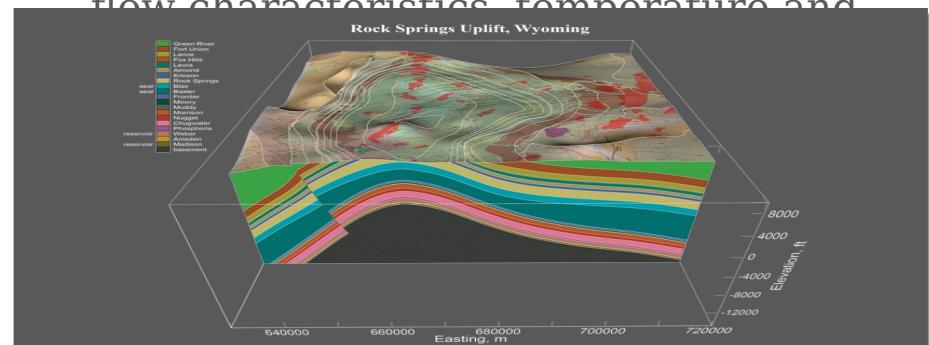
WSGS, UW, WY, and DOE-funded research identified two high-potential CCUS sites in southwest Wyoming:
Rock Springs Uplift and Moxa Arch



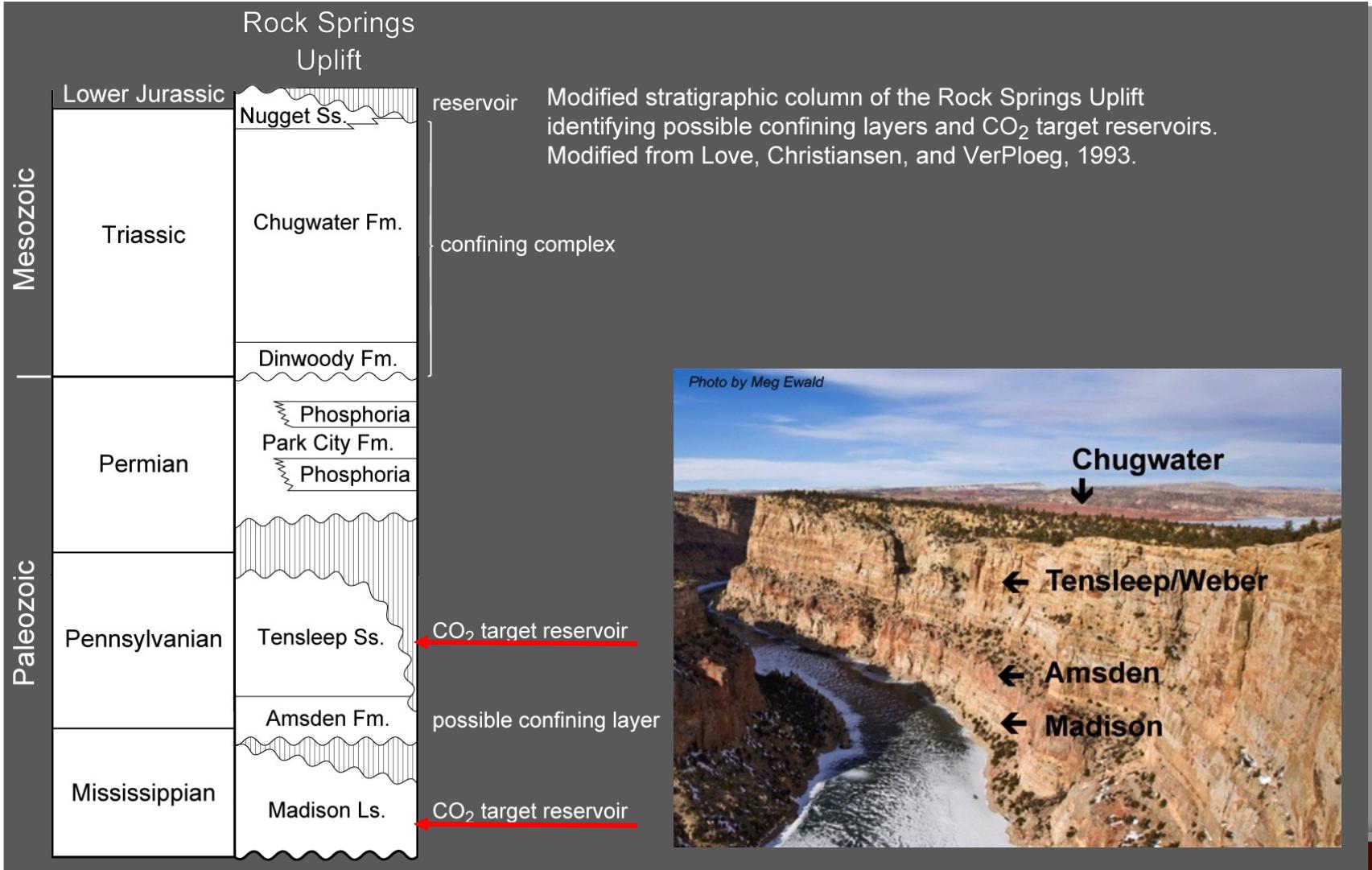
The Rock Springs Uplift: an Outstanding Geological CO₂ Storage Site in SW Wyoming



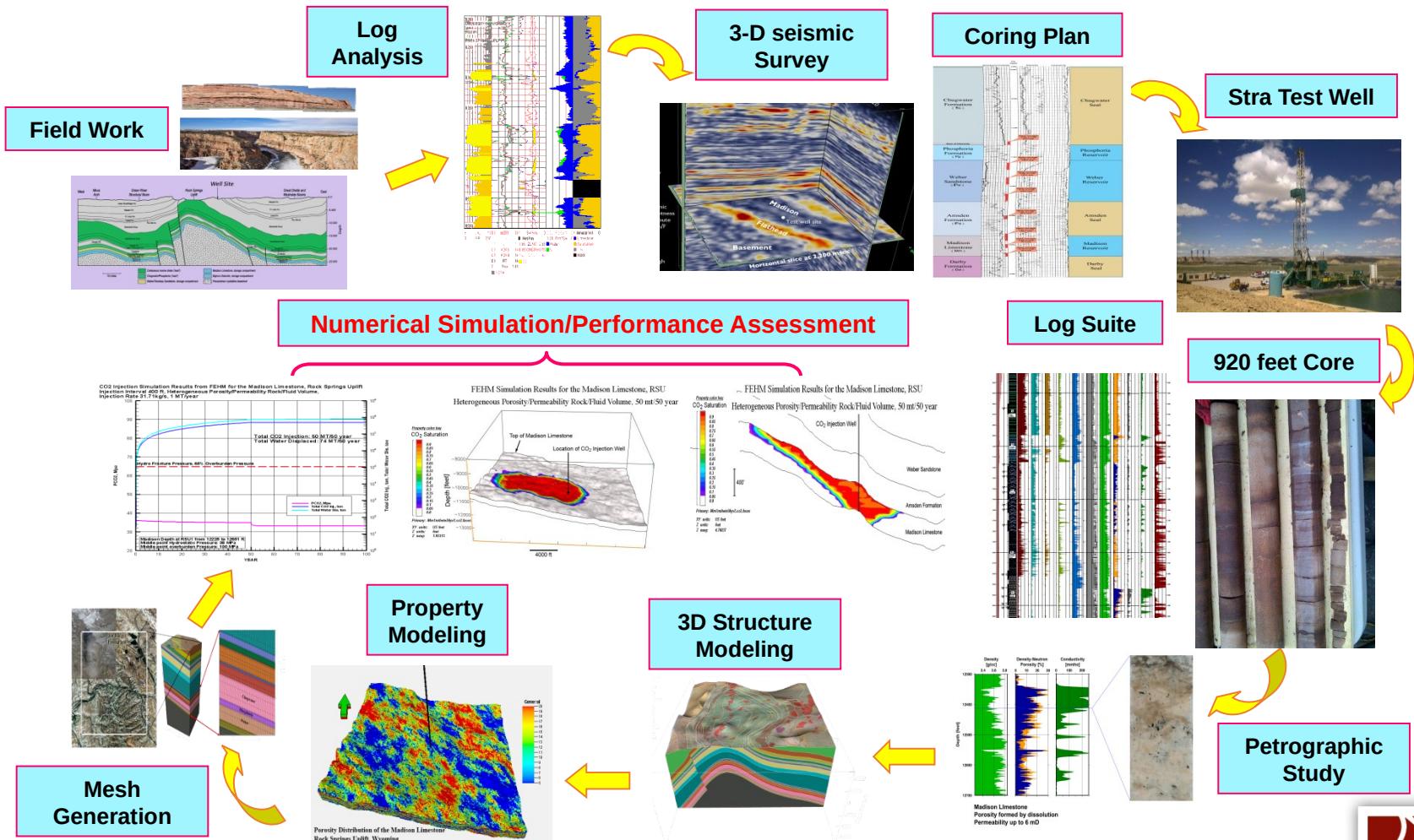
- Multiple thick saline aquifer sequences overlain by thick sealing lithologies (8000 feet of vertical separation between CO₂ storage reservoirs and fresh water aquifers)
- Doubly-plunging anticline characterized by more than 10,000 feet of closed structural relief
- Huge area (50 x 35 miles)
- Required reservoir conditions, including, but not limited to fluid chemistry, porosity (pore space), fluid-flow characteristics, temperature and



Targeted Geological CO₂ Storage Saline Formations



Work Flow for Geological CO₂ Storage Site Characterization

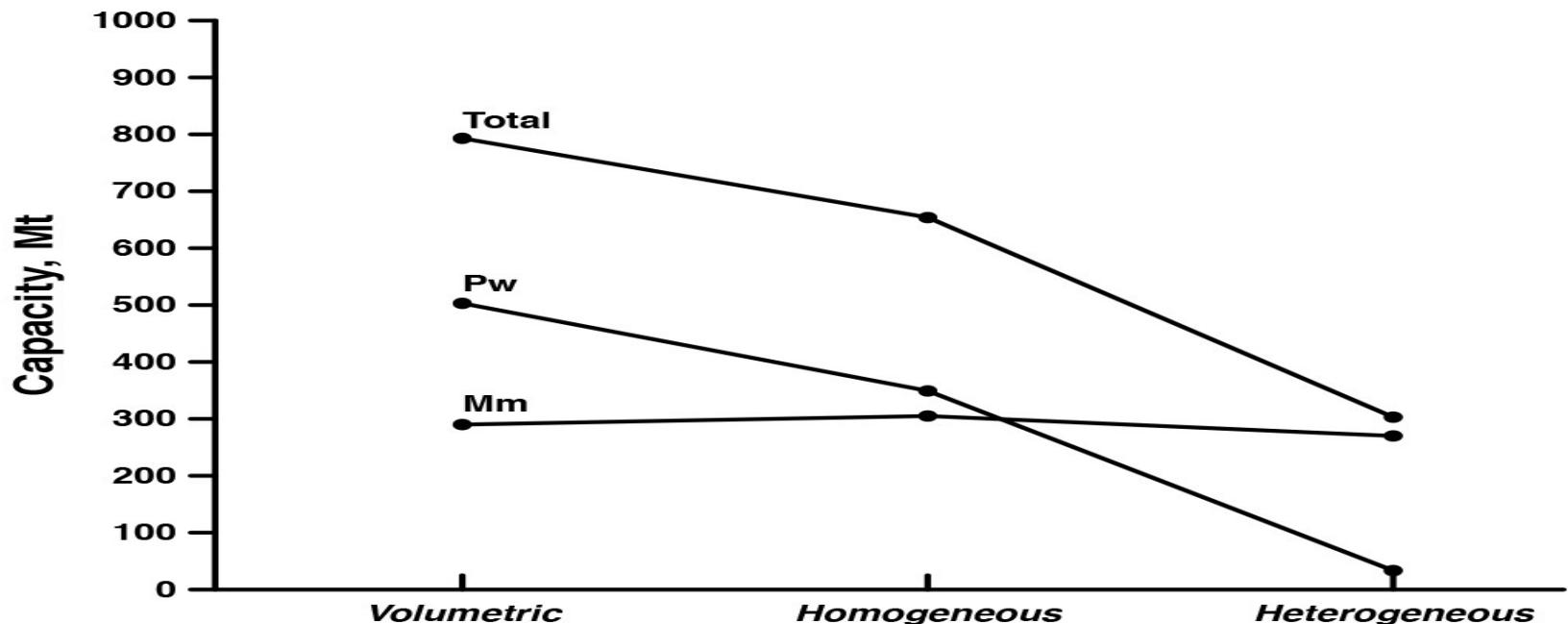


Comparison of CO₂ Storage Capacity Utilizing 3 Different Techniques – 5 mi x 5 mi storage domain

| Formation | Static Volumetric Approach ¹ | | | Dynamic Numerical Simulation ² Homogenous Reservoir Model | | | Dynamic Numerical Simulation ² Heterogeneous Reservoir Model | | |
|-----------|---|--------------|----------------------|---|----------------------|-----------------|--|----------------------|-----------------|
| | Area, km ² | Thickness, m | Storage Capacity, Mt | Injection Rate, Mt/y | Storage Capacity, Mt | Injection Wells | Injection Rate, Mt/y | Storage Capacity, Mt | Injection Wells |
| Weber | 64 | 210 | 503 | 1.0 | 350 | 7 | 0.3 | 33 | 7 |
| Madison | 64 | 120 | 290 | 1.0 | 305 | 6 | 1.0 | 270 | 6 |

1 – USGS Open File Report 2009-1035

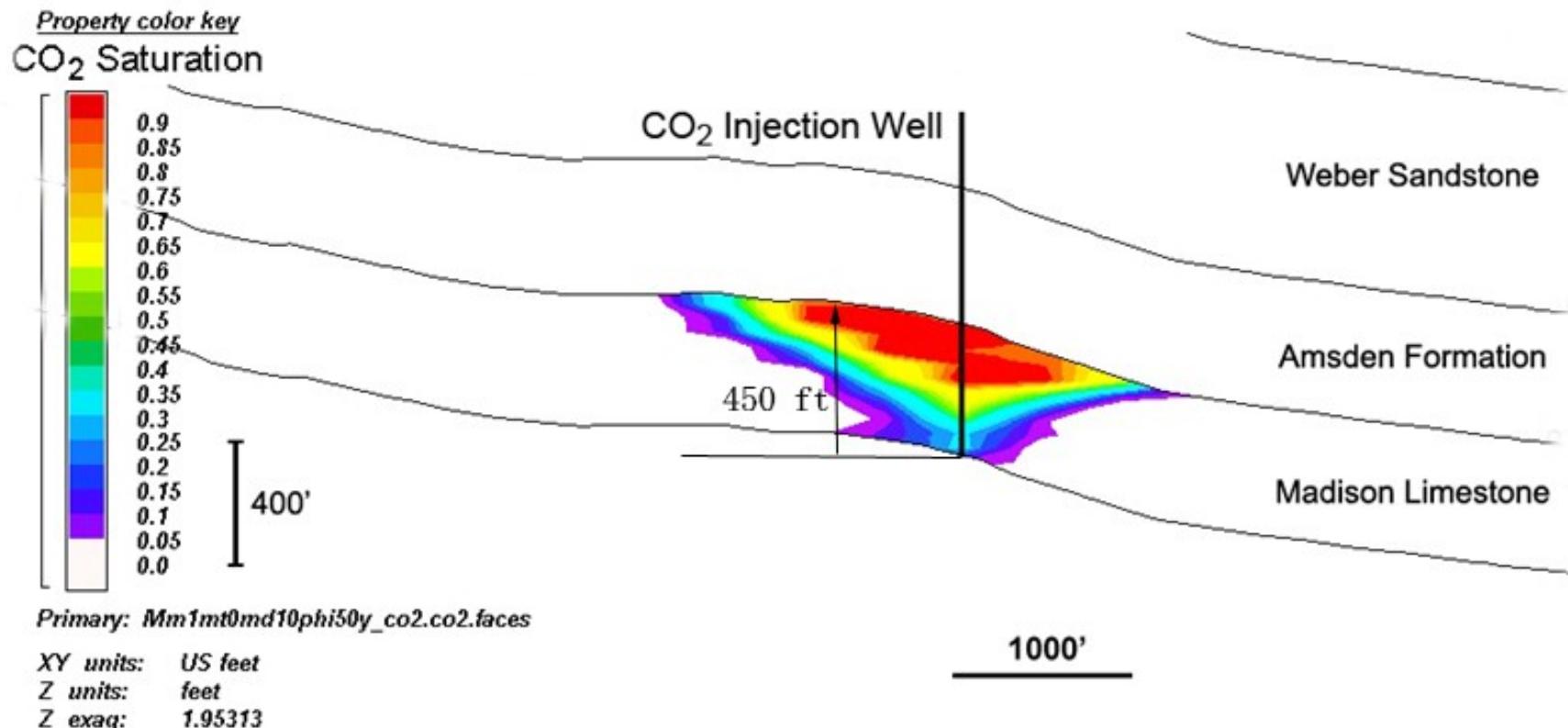
2 – FEHM, Los Alamos National Laboratory



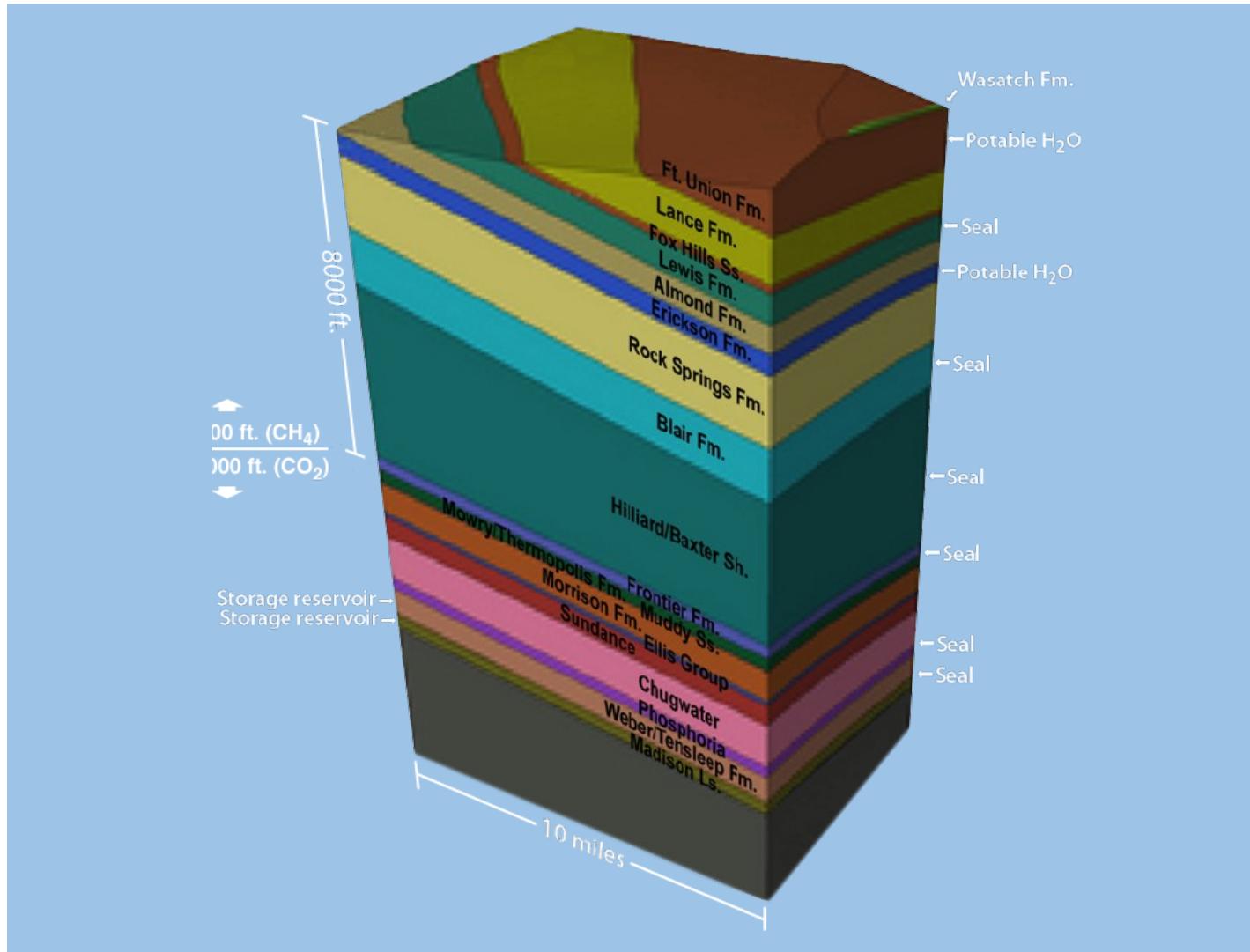
FEHM Simulation Results for the Madison Limestone, RSU

Homogeneous Porosity/Permeability Rock/Fluid Volume

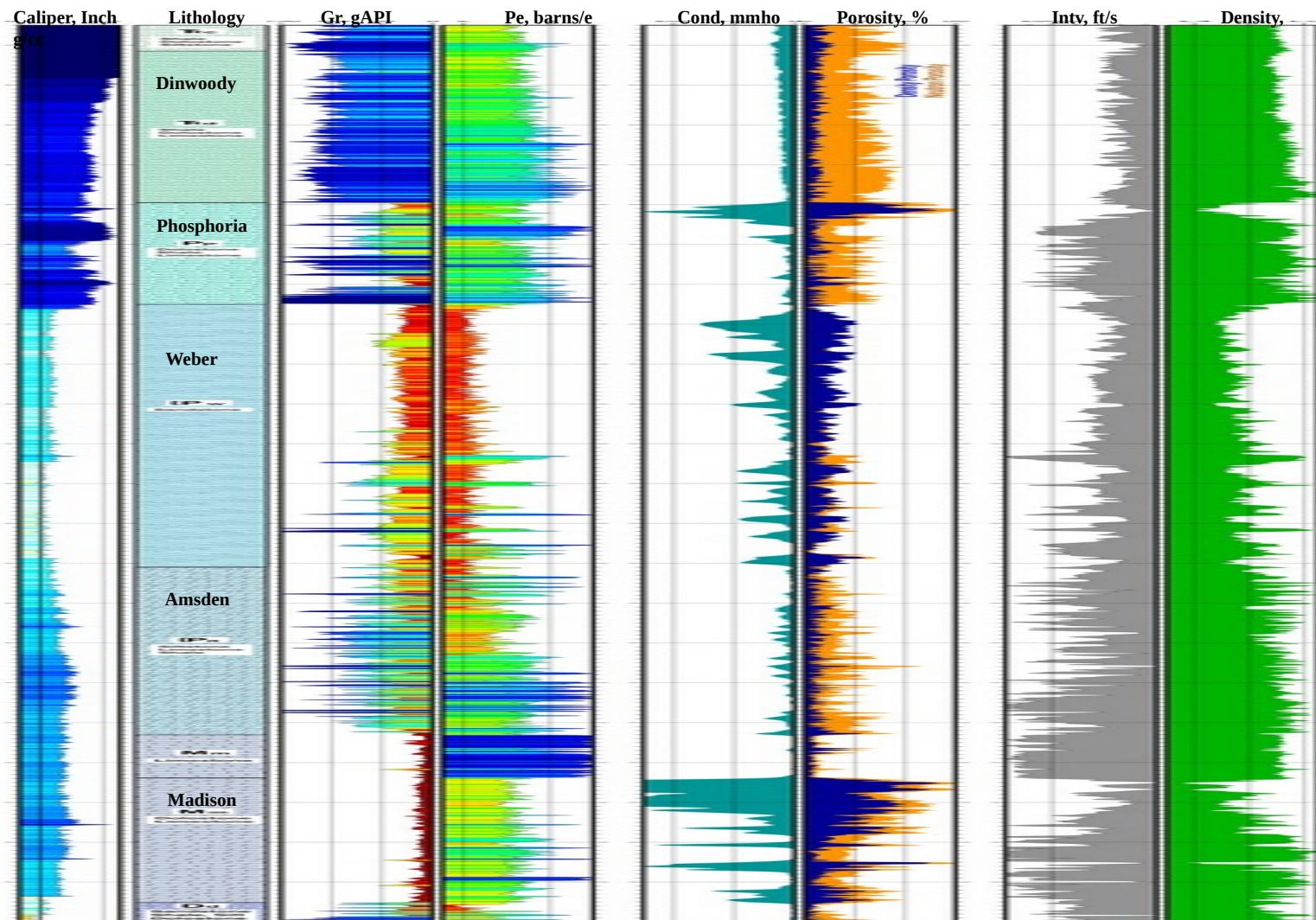
Porosity 10%, Permeability 10 md, 50 Mt/50 years



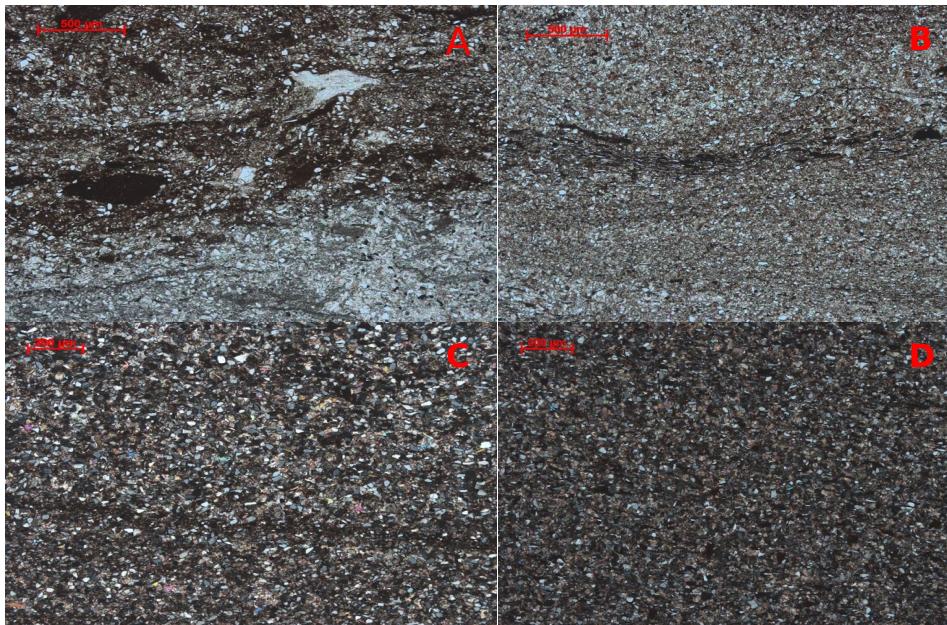
Rock Springs Uplift Hydrostratigraphic System



Stratigraphic Column and Select Petrophysical Logs for RSU #1

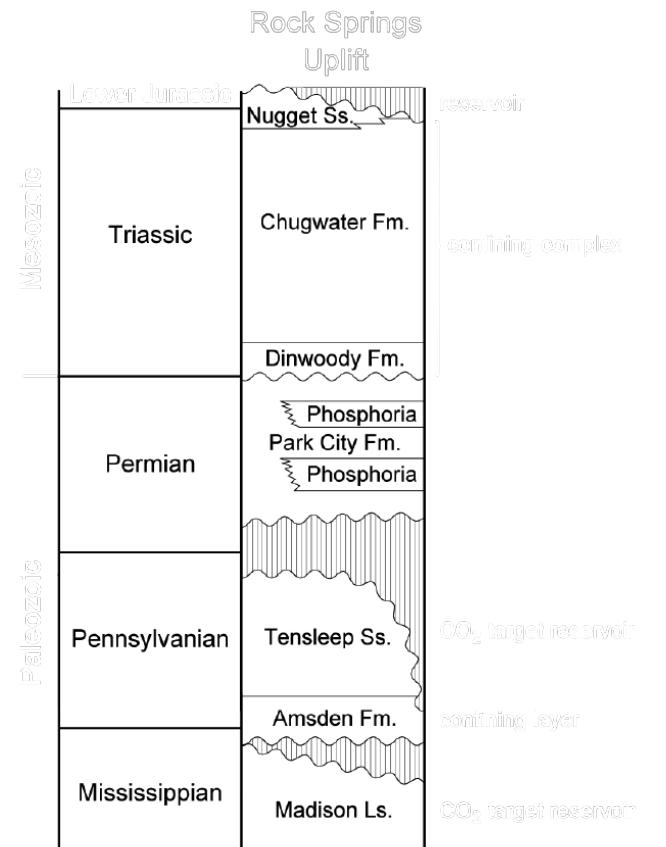


Chugwater Group (Primary Seal for the Weber Sandstone)



Microphotographs of Chugwater Group siltstones at depths of A: 10,627.8', B: 10,662.8', C: 10,682.1' and D: 10,601.9' clockwise from top left. C and D represent typical, laminated siltstones of the Chugwater Group.

Petrographic porosity is negligible due to cementation. A: shows mud intraclasts, anhydrite nodules, and a contact at a reduction zone (bottom part of slide, light-colored). Calcite increases in the reduction zones as it replaces anhydrite. B: shows increased illite compositions along a minor mineralization band.



Modified stratigraphic column of the Rock Springs Uplift identifying confining layers and CO₂ target reservoirs
Modified from Love, Christiansen, and VerPloeg, 1983.

$$\text{Porosity (Hg)} = 3\%$$
$$\text{Permeability} = 0.003 \text{ md}$$



Chugwater Group Siltstones



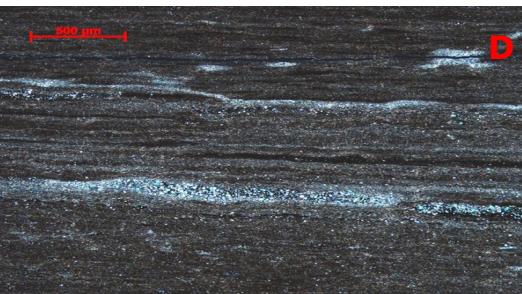
Porosity (Hg) = 2%
Permeability = 0.005 md



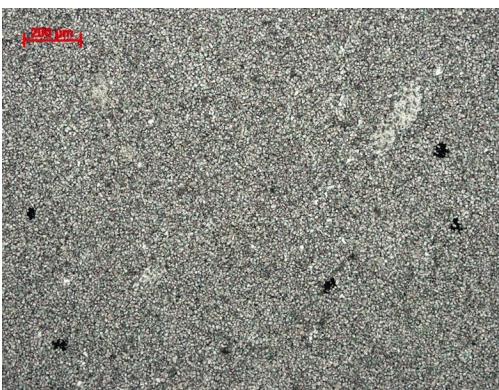
Porosity (Hg) = 2%
Permeability = 0.003 md



Amsden Formation (Primary Seal for the Madison limestone)



Porosity (Hg), 2%
Permeability, 0.003 md



Microphotographs of the Amsden Formation at depths of A: 12,203', B: 12,218.7', C: 12,199', and D: 12,209' clockwise from top left. Note the heterogeneity in lithologies from the fossiliferous limestone in A to the fine-grained siltstone in C to the bimodal sandstone in D. All slides have some evidence of secondary mineralization and deep burial alteration, figures succinctly displays a contact between neomorphic calcite (right portion of slide, reddish) and the primary micritic limestone with chert cements. A thin, dark dissolution band of insoluble minerals separates the facies.

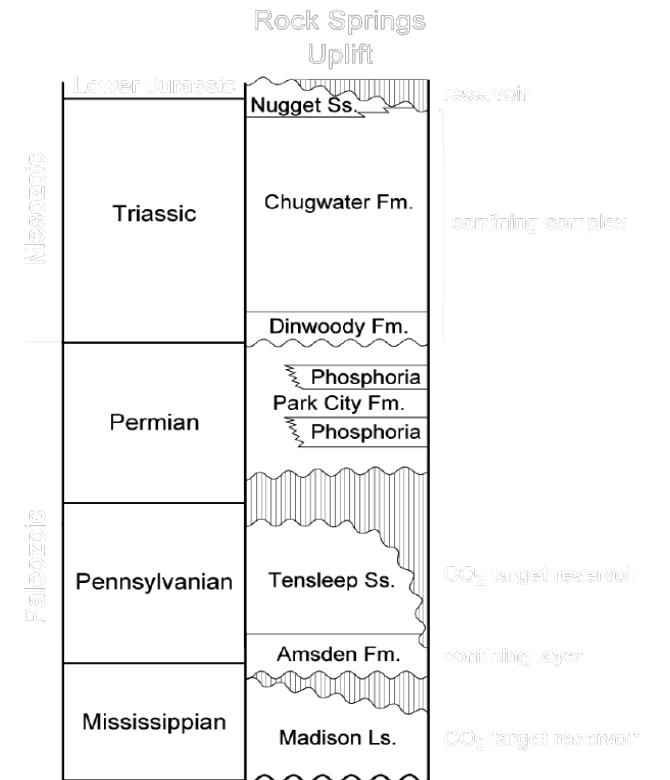
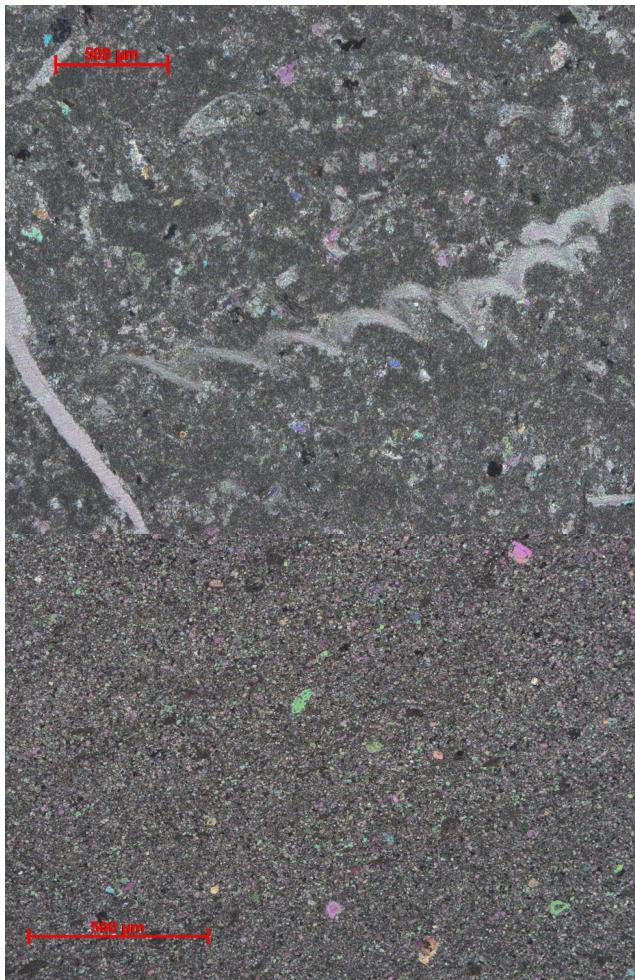


The Most Up-Portion of the Madison Limestone (Primary Seal)

12,250.0 ft.



Typical fossiliferous micrites in the Madison limestone facies and depths of A: 12,249.8' and B: 12,233'. This facies is typified by mainly primary features, lack of developed pore space, and micritic cements.

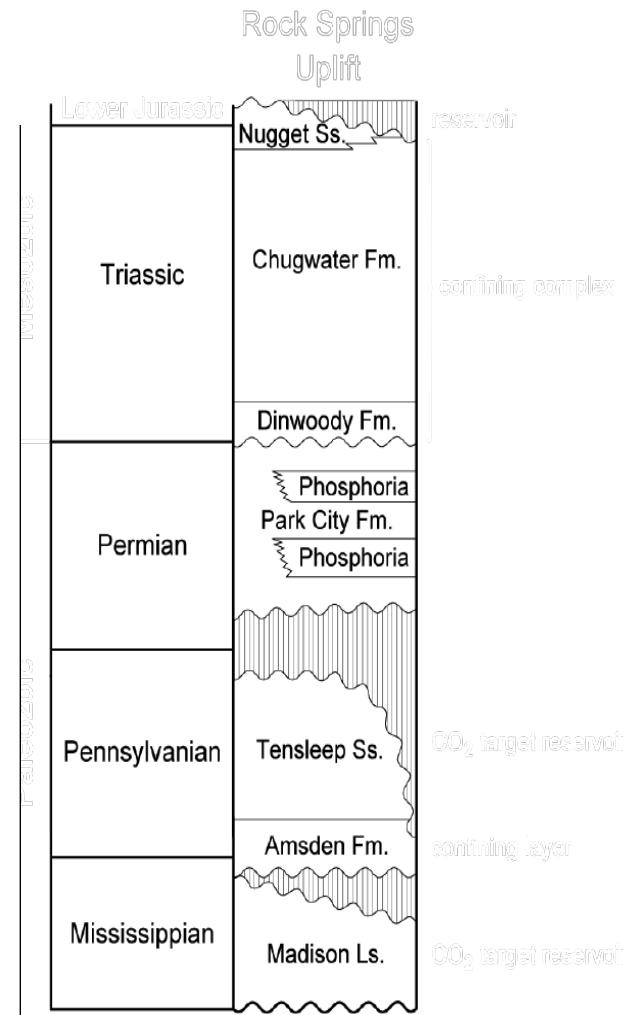
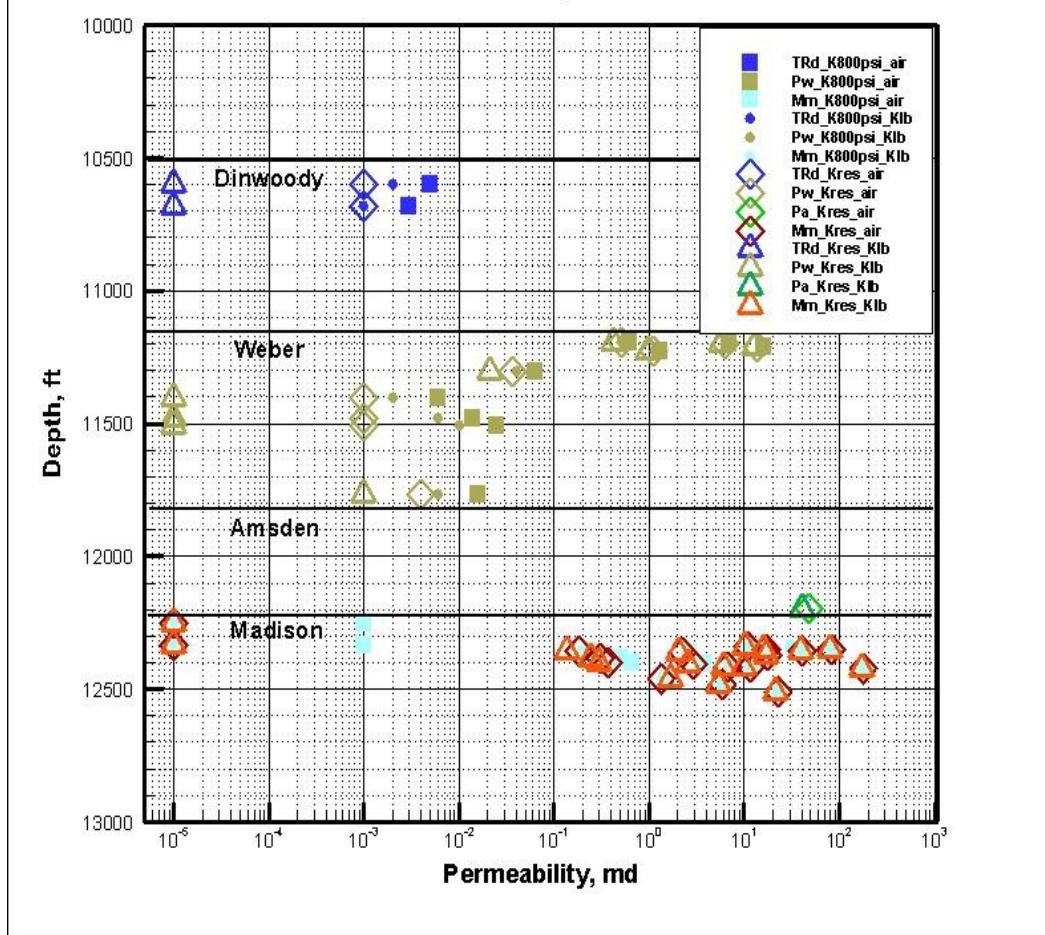


Modified stratigraphic column of the Rock Springs Uplift identifying confining layers and CO₂ target reservoirs.
Modified from Love, Chris Jameson, and VerPlank, 1993.

Porosity (Hg) = 1.9%
Permeability = 0.001 md



The Air and Klinkenberg Permeabilities of Core from RSU #1



Modified stratigraphic column of the Rock Springs Uplift
Identifying confining layers and CO₂ target reservoirs.
Modified from Love, Christiansen, and VerPlanck, 1993.



Entry Pressures and Column Height

The subsurface hydrocarbon-water or CO₂-water entry pressure values can be derived from the mercury entry pressure values by using following equation (Purcell, 1949, Schowalter, 1979):

$$P_{c_res} = P_{c_ma} * \frac{\gamma_{res} * \cos\theta_{res}}{\gamma_{ma} * \cos\theta_{ma}}$$

The height of a hydrocarbon or supercritical CO₂ column that a confining layer can hold, can be determined by using following equation (Smith, 1966, Schowalter, 1979):

$$H = \frac{P_{ds} - P_{dr}}{(\rho_w - \rho_{co2}) * 0.433}$$



Parameters Used for the Displacement Pressure Calculations

| Parameters used for Displacement Pressure Calculation | | | | | |
|---|-----|-------------------------|--|-------|--------|
| Laboratory IFT | | Height above free water | | | |
| Air/mercury IFT = | 485 | | | | |
| Gas/water IFT = | 72 | | | | |
| Gas/Oil IFT = | 24 | | | | |
| Oil/Water IFT = | 48 | density brine = | | g/cm3 | psi/ft |
| | | density of oil = | | 1.080 | 0.468 |
| | | density of gas = | | 0.840 | 0.364 |
| | | | | 0.200 | 0.087 |
| Reservoir IFT | | | | | |
| Gas/water IFT = | 50 | | | | |
| Oil/Water IFT = | 30 | | | | |
| CO2/Water IFT = | 30 | gas/water coef = | | 2.62 | |
| | | oil/water coef. = | | 9.62 | |
| Laboratory Contact Angle | | Cosine Contact Angle | | | |
| Air/Water | 0 | 1.000 | | | |
| Oil-Water | 30 | 0.866 | | | |
| Air-Mercury against rock | 140 | 0.766 | | | |
| Air-Oil | 0 | 1.000 | | | |
| Reservoir Contact Angle | | | | | |
| Water/Gas contact angle | 0 | 1.000 | | | |
| Water/Oil contact angle | 30 | 0.866 | | | |
| CO2/Water contact angle | 60 | 0.500 | | | |
| Laboratory IFT*Cosine Contact Angle | | | | | |
| Air/Water | 72 | | Intertek, 2014, Chun and Wilkinson | | |
| Oil-Water | 42 | | (1995), Yang et al. (2005), Dickson et al. | | |
| Air-Oil | 24 | | (2006), Chalbaud et al. (2006, 2009), | | |
| Air/Mercury | 372 | | Chiquet et al. (2007), Espinoza and | | |
| | | | Santamarina (2010), Wollenweber et al. | | |
| Reservoir IFT*Cosine Contact Angle | | | | | |
| Air/Water | 50 | | (2010), Daniel et al., (2009), Buursink et | | |
| Oil-Water | 26 | | al. (2011), silva et al. (2012), and Edlmann | | |
| CO2-water | 15 | | et al. (2013). | | |



Entry Pressures Derived from High-Pressure Mercury Injection Test Results (Lab Condition)

| Sample | Interval | Formation | Type | Grain | Porosity | Entry Pressure (lab) | | |
|--------|-------------|------------------|-----------|-------|----------|----------------------|---------|---------|
| | | | | | | A-Hg | G-W | O-W |
| | ID | ft | ID | g/cc | % | psi | psia | psia |
| 176 | 11725.9 | Weber 1 | CoLe Plug | 2.70 | 0.40 | 576.5 | 111.727 | 64.506 |
| 187 | 12178.1 | Amsden 1 | Core Plug | 2.91 | 5.89 | 146.6 | 28.402 | 16.398 |
| 200 | 12227.3 | Amsden 2 | Core Plug | 2.85 | 2.60 | 80.5 | 15.605 | 9.010 |
| 206 | 12301.0 | Madison | Core Plug | 2.74 | 1.90 | 3000.0 | 581.377 | 335.658 |
| 214 | 12333.9 | Madison 1 | Core Plug | 2.83 | | 3630.1 | 703.488 | 406.159 |
| B1 | 6300-6330 | Baxter 1 | Cuttings | 2.59 | | 390.4 | 75.661 | 43.683 |
| B2 | 7680-7710 | Baxter 2 | Cuttings | 2.57 | | 217.3 | 42.102 | 24.307 |
| B3 | 7590-7620 | Baxter 3 | Cuttings | 2.49 | | 430.6 | 83.452 | 48.181 |
| M1 | 8130-8160 | Mowry 1 | Cuttings | 2.51 | | 701.0 | 135.854 | 78.435 |
| M1 | 8220-8250 | Mowry 2 | Cuttings | 2.50 | | 1032.4 | 200.075 | 115.513 |
| GS1 | 9190-9200 | Gypsum Springs 1 | Cuttings | 2.59 | | 850.3 | 164.790 | 95.142 |
| P1 | 11040-11050 | Phosphoria 1 | Cuttings | 2.71 | | 354.5 | 68.696 | 39.661 |
| P2 | 11140-11150 | Phosphoria 2 | Cuttings | 2.65 | | 389.7 | 75.530 | 43.607 |
| 1 | 10601.9 | Red Peak | Core Plug | | 1.60 | 939.7 | 182.107 | 105.139 |
| 4 | 10605.9 | Red Peak | Core Plug | | 1.60 | 1140.0 | 220.923 | 127.550 |
| 16 | 10656.4 | Red Peak | Core Plug | | 1.00 | 2719.0 | 526.922 | 304.218 |
| 18 | 10682.1 | Red Peak | Core Plug | | 1.20 | 1521.0 | 294.758 | 170.179 |
| 26 | 11209.9 | Weber | Core Plug | | 8.10 | 7.8 | 1.512 | 0.873 |
| 27 | 11227.1 | Weber | Core Plug | | 7.60 | 35.0 | 6.783 | 3.916 |
| 45 | 11766.8 | Weber | Core Plug | | 1.30 | 1034.0 | 200.381 | 115.690 |
| 53 | 12197.4 | Amsden | Core Plug | | 5.80 | 1381.0 | 267.627 | 154.515 |
| 59 | 12250.0 | Madison | Core Plug | | 1.30 | 1254.0 | 243.016 | 140.305 |
| 72 | 12348.9 | Madison | Core Plug | | 18.10 | 22.0 | 4.263 | 2.461 |
| 79 | 12354.7 | Madison | Core Plug | | 23.50 | 35.0 | 6.783 | 3.916 |
| 99 | 12399.0 | Madison | Core Plug | | 11.60 | 37.0 | 7.170 | 4.140 |
| 106 | 12415.1 | Madison | Core Plug | | 18.50 | 9.1 | 1.764 | 1.018 |
| 110 | 12480.5 | Madison | Core Plug | | 11.80 | 5.1 | 0.984 | 0.568 |

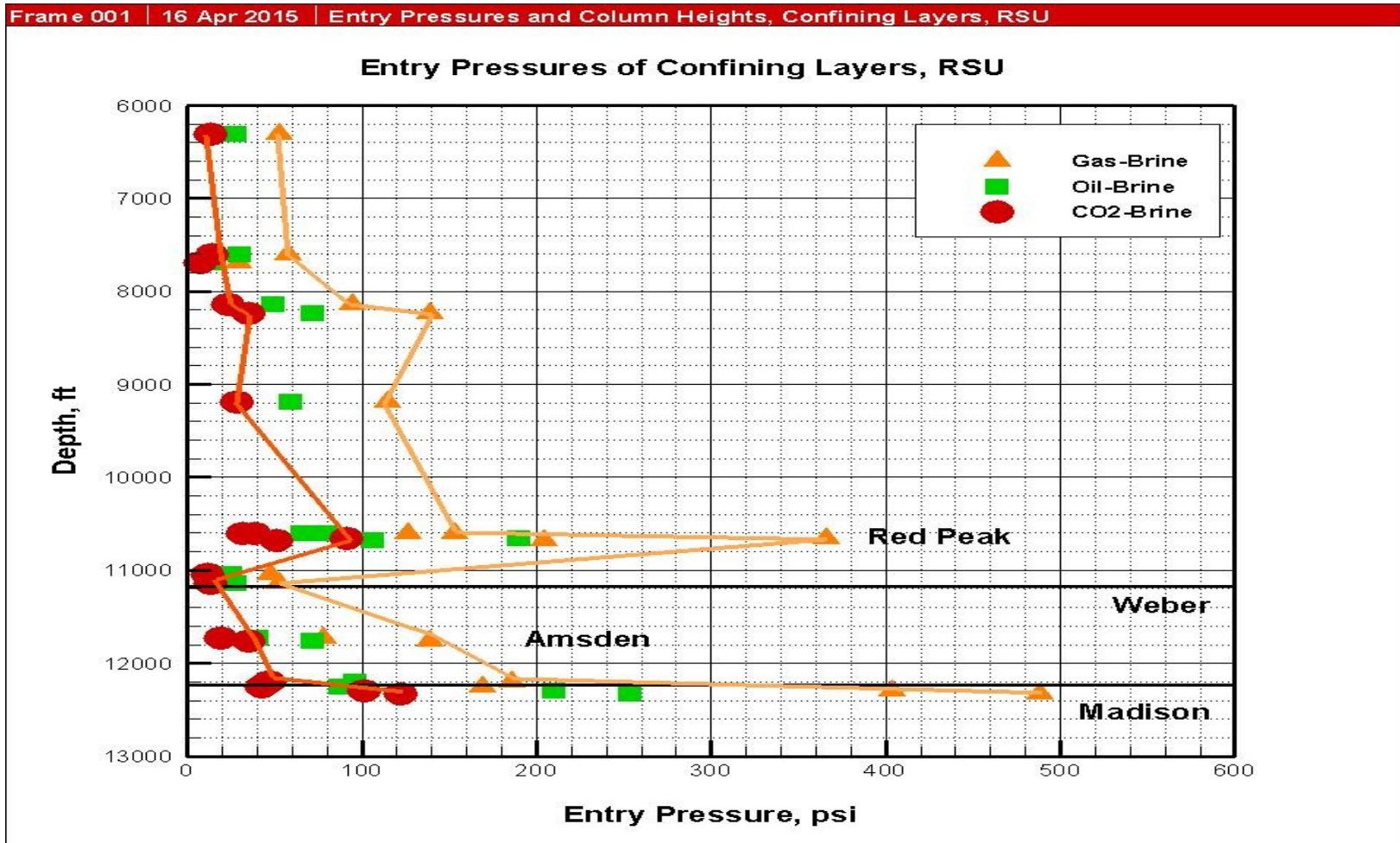


Entry Pressures Derived from High-Pressure Mercury Injection Test Results (Reservoir Condition)

| | Interval | | Sample | Grain | Porosity | Entry Pressure (res) | | | |
|--------|-------------|------------------|-----------|---------|----------|----------------------|---------|-----------|---------|
| Sample | Depth | Formation | Type | Density | Helium | G-W | O-W | O_W(calc) | scCO2-W |
| ID | ft | ID | | g/cc | % | | | | |
| 176 | 11725.9 | Weber 1 | CoLe Plug | 2.70 | 0.40 | 77.588 | 40.316 | 40.32 | 19.397 |
| 187 | 12178.1 | Amsden 1 | Core Plug | 2.91 | 5.89 | 19.724 | 10.249 | 10.25 | 4.931 |
| 200 | 12227.3 | Amsden 2 | Core Plug | 2.85 | 2.60 | 10.837 | 5.631 | 5.63 | 2.709 |
| 206 | 12301.0 | Madison | Core Plug | 2.74 | 1.90 | 403.734 | 209.786 | 209.79 | 100.934 |
| 214 | 12333.9 | Madison 1 | Core Plug | 2.83 | | 488.533 | 253.849 | 253.85 | 122.133 |
| B1 | 6300-6330 | Baxter 1 | Cuttings | 2.59 | | 52.543 | 27.302 | 27.30 | 13.136 |
| B2 | 7680-7710 | Baxter 2 | Cuttings | 2.57 | | 29.237 | 15.192 | 15.19 | 7.309 |
| B3 | 7590-7620 | Baxter 3 | Cuttings | 2.49 | | 57.953 | 30.113 | 30.11 | 14.488 |
| M1 | 8130-8160 | Mowry 1 | Cuttings | 2.51 | | 94.343 | 49.022 | 49.02 | 23.586 |
| M1 | 8220-8250 | Mowry 2 | Cuttings | 2.50 | | 138.941 | 72.196 | 72.20 | 34.735 |
| GS1 | 9190-9200 | Gypsum Springs 1 | Cuttings | 2.59 | | 114.438 | 59.464 | 59.46 | 28.609 |
| P1 | 11040-11050 | Phosphoria 1 | Cuttings | 2.71 | | 47.705 | 24.788 | 24.79 | 11.926 |
| P2 | 11140-11150 | Phosphoria 2 | Cuttings | 2.65 | | 52.451 | 27.254 | 27.25 | 13.113 |
| 1 | 10601.9 | Red Peak | Core Plug | | 1.60 | 126.463 | 65.712 | 65.71 | 31.616 |
| 4 | 10605.9 | Red Peak | Core Plug | | 1.60 | 153.419 | 79.719 | 79.72 | 38.355 |
| 16 | 10656.4 | Red Peak | Core Plug | | 1.00 | 365.918 | 190.136 | 190.14 | 91.479 |
| 18 | 10682.1 | Red Peak | Core Plug | | 1.20 | 204.693 | 106.362 | 106.36 | 51.173 |
| 26 | 11209.9 | Weber | Core Plug | | 8.10 | 1.050 | 0.545 | 0.55 | 0.262 |
| 27 | 11227.1 | Weber | Core Plug | | 7.60 | 4.710 | 2.448 | 2.45 | 1.178 |
| 45 | 11766.8 | Weber | Core Plug | | 1.30 | 139.154 | 72.306 | 72.31 | 34.788 |
| 53 | 12197.4 | Amsden | Core Plug | | 5.80 | 185.852 | 96.572 | 96.57 | 46.463 |
| 59 | 12250.0 | Madison | Core Plug | | 1.30 | 168.761 | 87.691 | 87.69 | 42.190 |
| 72 | 12348.9 | Madison | Core Plug | | 18.10 | 2.961 | 1.538 | 1.54 | 0.740 |
| 79 | 12354.7 | Madison | Core Plug | | 23.50 | 4.710 | 2.448 | 2.45 | 1.178 |
| 99 | 12399.0 | Madison | Core Plug | | 11.60 | 4.979 | 2.587 | 2.59 | 1.245 |
| 106 | 12415.1 | Madison | Core Plug | | 18.50 | 1.225 | 0.636 | 0.64 | 0.306 |
| 110 | 12480.5 | Madison | Core Plug | | 11.80 | 0.684 | 0.355 | 0.36 | 0.171 |



Entry Pressures Derived from High-Pressure Mercury Injection Test Results (Reservoir Condition)

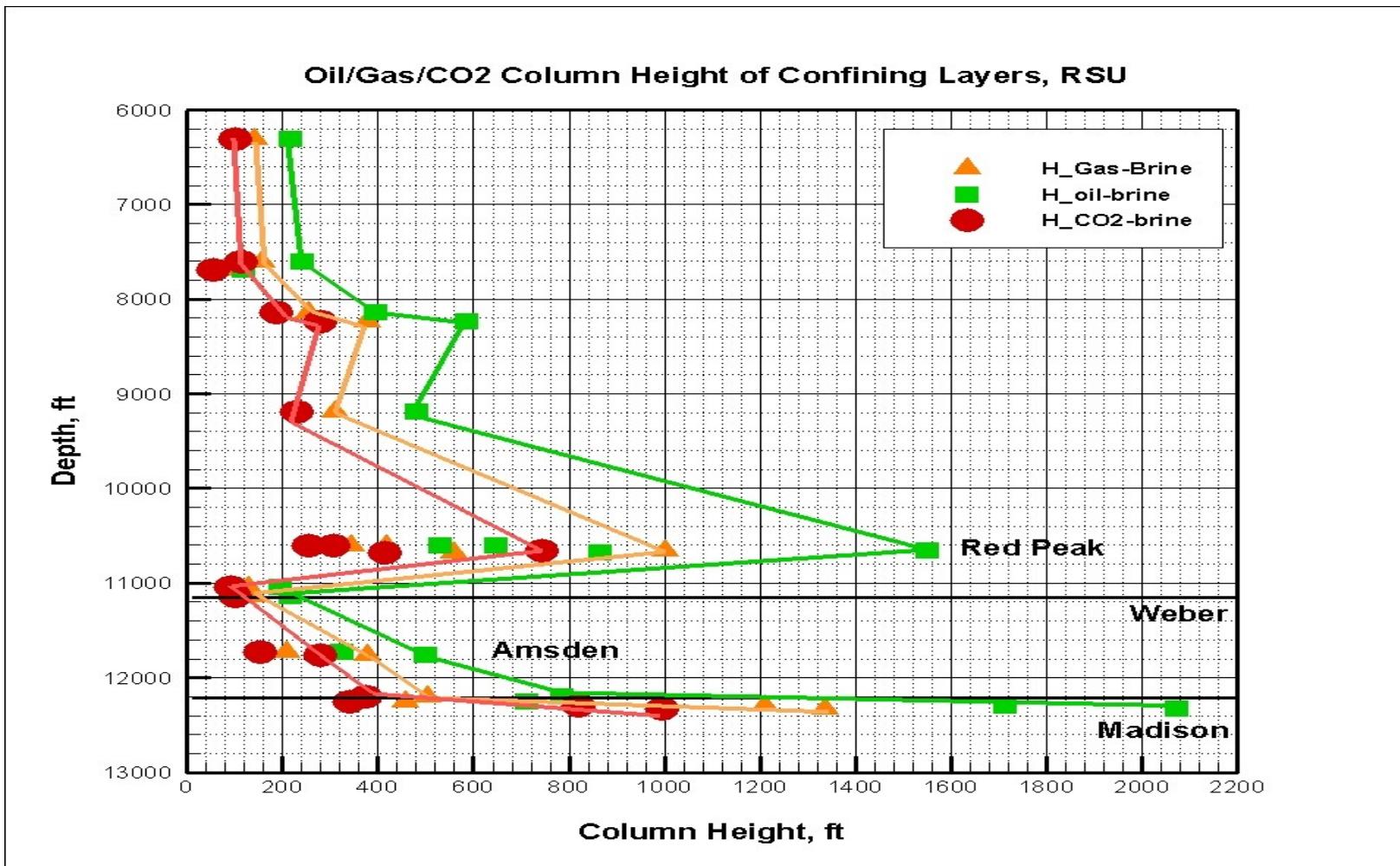


Column Height Derived from High-Pressure Mercury Injection Test Results (Reservoir Condition)

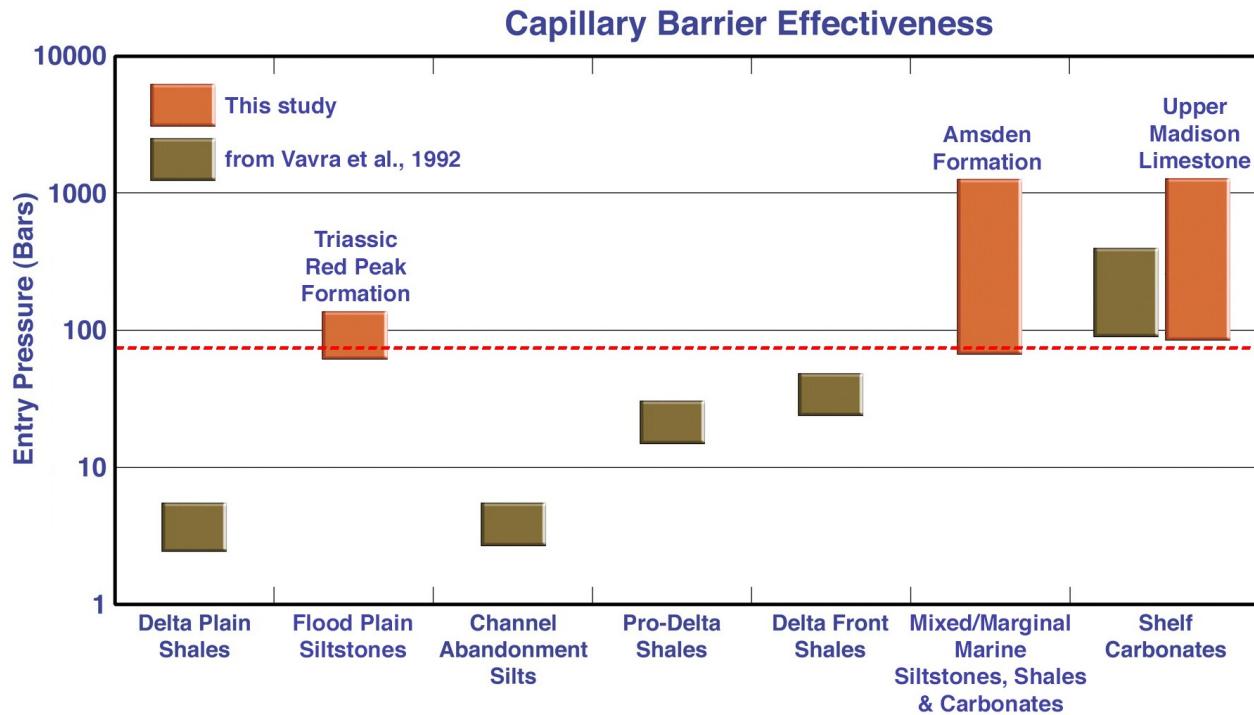
| Sample ID | Interval Depth ft | Formation ID | Sample Type | Column Height (res) | | |
|--------------------------|-------------------|--------------|-------------|---------------------|---------|----------|
| | | | | G-W ft | O-W ft | CO2-W ft |
| Containment Layer | | | | | | |
| 214.00 | 12333.90 | Madison | Core Plug | 1335.15 | 2072.96 | 994.26 |
| 206.00 | 12301.00 | Madison | Core Plug | 1209.58 | 1712.17 | 820.71 |
| 16.00 | 10656.40 | Red Peak | Core Plug | 1001.93 | 1551.25 | 743.28 |
| 18.00 | 10682.10 | Red Peak | Core Plug | 558.66 | 865.16 | 413.19 |
| 53.00 | 12197.40 | Amsden | Core Plug | 502.97 | 784.92 | 374.55 |
| 59.00 | 12250.00 | Madison | Core Plug | 455.98 | 712.19 | 339.56 |
| 4.00 | 10605.90 | Red Peak | Core Plug | 417.69 | 646.97 | 308.21 |
| 45.00 | 11766.80 | Weber | Core Plug | 378.47 | 500.98 | 279.01 |
| M1 | 8220-8250 | Mowry 2 | Cuttings | 377.89 | 585.36 | 278.57 |
| 1.00 | 10601.90 | Red Peak | Core Plug | 343.58 | 532.26 | 253.02 |
| GS1 | 9190-9200 | Gypsum S | Cuttings | 310.52 | 481.09 | 228.40 |
| M1 | 8130-8160 | Mowry 1 | Cuttings | 255.27 | 395.58 | 187.26 |
| 176.00 | 11725.90 | WebeR 1 | CoLe Plug | 209.20 | 324.28 | 152.96 |
| B3 | 7590-7620 | Baxter 3 | Cuttings | 155.22 | 240.72 | 112.76 |
| B1 | 6300-6330 | Baxter 1 | Cuttings | 140.34 | 217.70 | 101.68 |
| P2 | 11140-111 | Phosphori | Cuttings | 140.09 | 217.31 | 101.49 |
| P1 | 11040-110 | Phosphori | Cuttings | 127.04 | 197.11 | 91.78 |
| B2 | 7680-7710 | Baxter 2 | Cuttings | 76.27 | 118.52 | 53.96 |



Column Height Derived from High-Pressure Mercury Injection Test Results (Reservoir Condition)



Displacement Pressures of Selected Sealing Units Relative to Lithologies



The dashed line indicates displacement pressure needed to retain a 300' column of injected gas.

From J.F. McLaughlin, et al., 2014



Remarks

- For the targeted Paleozoic storage reservoirs, the confining layers are shale/siltstones of the Chugwater Group (Red Peak Fm.) and the Amsden Formation, and the most upper portion of the Madison Limestone.
- The CO₂ column heights that the various confining layers at the RSU can hold range from 50 ft to 990 ft.
- CO₂ column heights (held by same confining layer) are only about half of the height of an oil column, and three-quarters of the gas column.
- It is potentially disastrous risk to assume that a confining layer which has successfully trapped hydrocarbons over million years, could also contain similar volumes of injected CO₂.
- CO₂ injection simulations for the Madison Limestone and Weber Sandstone reservoirs indicate that CO₂ column heights could rise to 500 ft in the Madison Limestone and 400 ft in the Weber Sandstone. This study shows that confining layers at the RSU storage site have adequate sealing capacity to safely hold the CO₂ columns after injected 50 Mt of supercritical CO₂ in the Madison Limestone and the Weber Sandstone.



Acknowledgement

We would like to acknowledge the support
of DOE (DE-FE0009202) in funding
and guiding this project

