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<u>WMTC Certification</u>	
➤ Administered by the University of Wyoming & WYDOT	
➤ Recognized by State of Wyoming	
➤ Valid for 5 years ( <i>must pass all three exams</i> )	
➤ Asphalt Exam ( <a href="#">take online</a> )	
➤ Multiple choice/True-False Questions (open book & notes)	
➤ Covers asphalt fundamentals & WYDOT Specifications	
➤ To Pass: 70% overall score or higher	
➤ Density Random Number Selection Exam ( <a href="#">take online</a> )	
➤ 10 Multiple choice/True-False Questions (open book & notes)	
➤ Covers WYDOT testing and procedures	
➤ To Pass: at least 7 questions should be answered correctly	
➤ Asphalt Testing Performance Exam covering ( <a href="#">take at WYDOT</a> )	
➤ Pass/Fail Exam: 2 tries per test (closed book & notes)	

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<u>Asphalt Characteristics</u>	
➤ Black cementing material	
➤ Solid or semisolid consistency	
➤ Primarily hydrocarbons	
➤ Consistency – temperature dependent	
➤ Viscoelastic	

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## Asphalt Sources

- Natural asphalt
- Petroleum asphalt

Section 1 - 4

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## Petroleum Asphalt Production

- Simple distillation
- Cracking

Section 1 - 5

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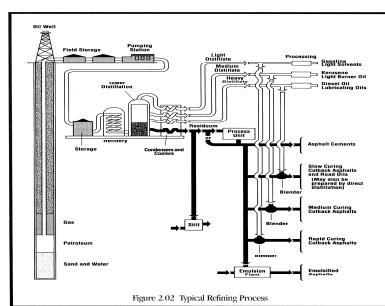
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## Typical Refining Process (Asphalt Institute)



Section 1 - 6

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## Asphalt Types

- Performance Graded Asphalt Binder
- Cutback asphalt
- Emulsified asphalt

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## Asphalt Uses

- Performance Graded Asphalt Binder
  - ▶ Asphalt binder pavement
  - ▶ Asphalt treated base
- Cutback asphalt
  - ▶ Cold mix
  - ▶ Prime coats

Section 1 - 8

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## Asphalt Uses (continued)

- Emulsified asphalt
  - ▶ Chip seals
  - ▶ Fog seals
  - ▶ Slurry seals
  - ▶ Microsurfacing
  - ▶ Tack coats

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## Asphalt Properties

### Chemical Properties

- **Composition** --- Hydrocarbons plus S, O, Mg, etc.
- **Asphaltenes** --- Solid phase
- **Maltenes** --- Liquid phase
  - **Resins** --- Heavy liquids
  - **Oils** --- Light liquids

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### Chemical Properties (continued)

- Aging changes proportions of asphaltenes and maltenes
- Aging is due to
  - Evaporation
  - Oxidation
  - Polymerization
- Changes during aging
  - Resins → Asphaltenes
  - Oils → Resins → Asphaltenes

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## Physical Properties

- Adhesion
- Temperature susceptibility
- Resistance to aging and hardening

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### **Handling and Storage**

- Avoid contact
- Wear appropriate equipment
- Know and follow safe procedures
- Stay upwind of hatch
- Avoid breathing fumes

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### **Handling and Storage (continued)**

- Apply cold water or ice
- Do not wipe
- Maintain temperature below flash point
- Monitor regularly
- Avoid mixing types

Section 1 - 14

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### **Temperature/Volume**

- Volume is corrected to 60°F for measurement and payment.
- To correct to 60°F you need:
  - ▶ Measured temperature
  - ▶ Specific gravity
  - ▶ Measured volume
  - ▶ Correction factor table
- Steps
  - ▶ With T and s.g. select C.F.
  - ▶ Calculate volume at 60°F
    - ▶  $V_{60} = (V_T) (C.F.)$

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### Asphalt Volume Correction Table - 1

Scope: The following table is used for Volume correction of asphaltic materials based on specific gravity and temperature. The temperature of 60°F (15.6°C) is customarily used as a standard for volume determination of asphalts. A unit volume of asphalt will change with each degree of temperature change (Coefficient of Volumetric Expansion). The correction factor varies with the specific gravity. The table below is applicable for all asphaltic materials, including emulsions (undiluted).

**Example:** If the specific Gravity = 0.985 at 60°F (15.6°C) and the Volume Measured = 9,000 gal. (34,066L) at 180°F (82.2°C), then read the table where 180°F (82.2°C) and 1.000 intersect (0.985 is closer to 1.000 than 0.950), and the **Correction Factor** = **0.9633**. Therefore the Corrected Volume at 60°F (15.6°C) = 9,000 gal. X 0.9633 = 8,670 gal. (32,817 L)

CORRECTION FACTORS (to determine volume at 60°F)							
Temperature	°F	°C	0.800	0.850	0.900	0.950	
40	4.4	0.6985	0.9885	0.9705	1.0068	1.001	1.0055
42	5.6	0.6987	0.9887	0.9707	1.0061	1.0005	1.0050
44	6.7	0.6976	0.9868	0.9690	1.0054	1.0049	1.0044
46	7.8	0.6967	0.9859	0.9683	1.0047	1.0043	1.0033
48	8.9	0.6957	0.9851	0.9675	1.0041	1.0037	1.0033
50	10.1	0.6947	0.9842	0.9667	1.0034	1.0031	1.0025
52	11.1	0.6938	0.9834	0.9659	1.0027	1.0024	1.0022
54	12.2	0.6929	0.9825	0.9652	1.0020	1.0018	1.0017
56	13.3	0.6919	0.9817	0.9615	1.0014	1.0012	1.0011
58	14.4	0.6910	0.9808	0.9608	1.0008	1.0006	1.0006
60	15.6	0.6900	0.9800	0.9600	1.0000	1.0000	1.0000
62	16.7	0.6890	0.9792	0.9593	0.9994	0.9994	0.9994
64	17.8	0.6881	0.9783	0.9585	0.9986	0.9986	0.9986
66	18.9	0.6871	0.9775	0.9577	0.9980	0.9982	0.9983
68	20.0	0.6861	0.9766	0.9569	0.9973	0.9975	0.9976
70	21.1	0.6852	0.9758	0.9562	0.9966	0.9969	0.9972
72	22.2	0.6843	0.9749	0.9555	0.9959	0.9963	0.9967
74	23.3	0.6833	0.9741	0.9547	0.9953	0.9957	0.9961
76	24.4	0.6824	0.9732	0.9540	0.9946	0.9951	0.9956
78	25.6	0.6814	0.9724	0.9532	0.9939	0.9946	0.9950
80	26.7	0.6805	0.9715	0.9525	0.9932	0.9939	0.9945

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### Asphalt Volume Correction Table - 2

CORRECTION FACTORS (to determine volume at 60°F)									
Temperature	°F	°C	Specific Gravity at 60°F	0.800	0.850	0.900	0.950	1.000	1.050
28.8	8.0	0.69885	0.9889	0.9900	0.9919	0.9927	0.9933	0.9940	0.9946
30.0	8.3	0.69876	0.9880	0.9902	0.9912	0.9921	0.9928	0.9934	0.9940
30.2	8.5	0.69867	0.9871	0.9904	0.9914	0.9922	0.9930	0.9937	0.9943
32.2	10.0	0.69857	0.9873	0.9907	0.9923	0.9930	0.9937	0.9944	0.9951
34.4	11.4	0.69838	0.9865	0.9908	0.9922	0.9935	0.9946	0.9953	0.9960
36.4	12.8	0.69828	0.9848	0.9902	0.9927	0.9940	0.9950	0.9959	0.9969
37.8	13.3	0.69809	0.9831	0.9849	0.9926	0.9946	0.9958	0.9968	0.9978
39.2	14.5	0.69790	0.9814	0.9833	0.9931	0.9951	0.9964	0.9974	0.9984
40.4	15.6	0.69780	0.9805	0.9823	0.9939	0.9953	0.9966	0.9976	0.9987
42.2	17.3	0.69770	0.9797	0.9819	0.9937	0.9953	0.9967	0.9977	0.9987
43.3	18.3	0.69761	0.9789	0.9811	0.9931	0.9947	0.9961	0.9971	0.9980
45.0	19.4	0.69752	0.9781	0.9803	0.9929	0.9943	0.9959	0.9969	0.9979
46.4	20.5	0.69742	0.9772	0.9794	0.9917	0.9936	0.9950	0.9960	0.9970
47.6	21.7	0.69733	0.9765	0.9781	0.9904	0.9923	0.9943	0.9954	0.9964
48.8	22.8	0.69713	0.9746	0.9774	0.9897	0.9917	0.9934	0.9945	0.9954
50.0	24.0	0.69703	0.9738	0.9766	0.9886	0.9911	0.9930	0.9941	0.9950
51.1	25.1	0.69694	0.9729	0.9759	0.9878	0.9904	0.9923	0.9933	0.9943
53.3	27.3	0.69675	0.9712	0.9743	0.9870	0.9901	0.9921	0.9931	0.9941
54.4	28.4	0.69666	0.9703	0.9736	0.9863	0.9892	0.9916	0.9926	0.9936
56.6	30.5	0.69656	0.9695	0.9726	0.9856	0.9881	0.9909	0.9920	0.9930
58.7	32.6	0.69647	0.9687	0.9721	0.9849	0.9874	0.9905	0.9915	0.9925
60.8	34.7	0.69637	0.9679	0.9715	0.9841	0.9865	0.9895	0.9905	0.9915
62.9	36.8	0.69627	0.9670	0.9706	0.9836	0.9852	0.9884	0.9894	0.9904
64.1	38.0	0.69618	0.9661	0.9697	0.9827	0.9842	0.9873	0.9883	0.9893
66.2	39.2	0.69608	0.9653	0.9689	0.9817	0.9836	0.9865	0.9875	0.9885
68.3	41.3	0.69599	0.9645	0.9683	0.9808	0.9823	0.9852	0.9862	0.9872
70.4	43.4	0.69589	0.9637	0.9676	0.9793	0.9813	0.9842	0.9852	0.9862
72.5	45.5	0.69579	0.9629	0.9669	0.9784	0.9808	0.9837	0.9847	0.9857
74.6	47.6	0.69569	0.9621	0.9662	0.9775	0.9799	0.9827	0.9837	0.9847
76.7	49.7	0.69559	0.9613	0.9655	0.9766	0.9788	0.9816	0.9826	0.9836
78.8	51.8	0.69549	0.9605	0.9647	0.9757	0.9779	0.9805	0.9815	0.9825
80.9	53.9	0.69539	0.9597	0.9639	0.9748	0.9769	0.9796	0.9806	0.9816
83.0	56.0	0.69529	0.9589	0.9631	0.9739	0.9759	0.9785	0.9795	0.9805
85.1	58.1	0.69519	0.9581	0.9623	0.9730	0.9750	0.9776	0.9786	0.9796
87.2	59.2	0.69509	0.9573	0.9615	0.9721	0.9739	0.9764	0.9774	0.9784
89.3	61.3	0.69499	0.9565	0.9606	0.9711	0.9726	0.9751	0.9761	0.9771
91.4	63.4	0.69489	0.9557	0.9598	0.9701	0.9716	0.9741	0.9751	0.9761
93.5	65.5	0.69479	0.9549	0.9590	0.9686	0.9701	0.9726	0.9736	0.9746
95.6	67.6	0.69469	0.9541	0.9583	0.9676	0.9691	0.9716	0.9726	0.9736
97.7	69.7	0.69459	0.9533	0.9575	0.9666	0.9681	0.9705	0.9715	0.9725
99.8	71.8	0.69449	0.9525	0.9567	0.9656	0.9671	0.9695	0.9705	0.9715
101.9	73.9	0.69439	0.9517	0.9559	0.9646	0.9661	0.9685	0.9695	0.9705
104.0	76.0	0.69429	0.9509	0.9550	0.9636	0.9651	0.9675	0.9685	0.9695
106.1	78.1	0.69419	0.9501	0.9542	0.9626	0.9641	0.9665	0.9675	0.9685
108.2	80.2	0.69409	0.9493	0.9534	0.9616	0.9631	0.9655	0.9665	0.9675
110.3	82.3	0.69399	0.9485	0.9526	0.9597	0.9612	0.9636	0.9646	0.9656
112.4	84.4	0.69389	0.9477	0.9518	0.9588	0.9603	0.9627	0.9637	0.9647
114.5	86.5	0.69379	0.9469	0.9510	0.9579	0.9594	0.9618	0.9628	0.9638
116.6	88.6	0.69369	0.9461	0.9502	0.9570	0.9585	0.9609	0.9619	0.9629
118.7	90.7	0.69359	0.9453	0.9494	0.9564	0.9579	0.9603	0.9613	0.9623
120.8	92.8	0.69349	0.9445	0.9486	0.9555	0.9570	0.9594	0.9604	0.9614
122.9	94.9	0.69339	0.9437	0.9478	0.9546	0.9561	0.9585	0.9595	0.9605
125.0	97.0	0.69329	0.9429	0.9470	0.9537	0.9552	0.9577	0.9587	0.9597
127.1	99.1	0.69319	0.9421	0.9462	0.9528	0.9543	0.9568	0.9578	0.9588
129.2	101.2	0.69309	0.9413	0.9454	0.9519	0.9534	0.9559	0.9569	0.9579
131.3	103.3	0.69299	0.9405	0.9446	0.9510	0.9525	0.9550	0.9560	0.9570
133.4	105.4	0.69289	0.9397	0.9438	0.9499	0.9515	0.9540	0.9550	0.9560
135.5	107.5	0.69279	0.9389	0.9430	0.9491	0.9506	0.9531	0.9541	0.9551
137.6	109.6	0.69269	0.9381	0.9422	0.9483	0.9498	0.9523	0.9533	0.9543
139.7	111.7	0.69259	0.9373	0.9414	0.9475	0.9490	0.9515	0.9525	0.9535
141.8	113.8	0.69249	0.9365	0.9406	0.9467	0.9482	0.9507	0.9517	0.9527
143.9	115.9	0.69239	0.9357	0.9398	0.9459	0.9474	0.9499	0.9509	0.9519
146.0	118.0	0.69229	0.9349	0.9390	0.9451	0.9466	0.9491	0.9501	0.9511
148.1	120.1	0.69219	0.9341	0.9382	0.9443	0.9458	0.9479	0.9489	0.9499
150.2	122.2	0.69209	0.9333	0.9374	0.9435	0.9450	0.9474	0.9484	0.9494
152.3	124.3	0.69199	0.9325	0.9366	0.9427	0.9442	0.9467	0.9477	0.9487
154.4	126.4	0.69189	0.9317	0.9358	0.9419	0.9434	0.9459	0.9469	0.9479
156.5	128.5	0.69179	0.9309	0.9350	0.9411	0.9426	0.9450	0.9460	0.9470
158.6	130.6	0.69169	0.9301	0.9342	0.9403	0.9418	0.9442	0.9452	0.9462
160.7	132.7	0.69159	0.9293	0.9334	0.9395	0.9410	0.9434	0.9444	0.9454
162.8	134.8	0.69149	0.9285	0.9326	0.9386	0.9401	0.9425	0.9435	0.9445
164.9	136.9	0.69139	0.9277	0.9318	0.9368	0.9383	0.9407	0.9417	0.9427
167.0	139.0	0.69129	0.9269	0.9310	0.9359	0.9			

### Asphalt Volume Correction Table - 4

CORRECTION FACTORS (to determine volume at 60°F)						
Temperature	Specific Gravity at 60°F	0.800	0.850	0.900	0.950	1.000
236	111.4	0.9137	0.9236	0.9319	0.9389	0.9449
240	115.6	0.9137	0.9236	0.9319	0.9389	0.9501
244	119.8	0.9118	0.9219	0.9304	0.9376	0.9437
248	118.9	0.9108	0.9211	0.9297	0.9369	0.9431
252	123.1	0.9088	0.9194	0.9281	0.9356	0.9419
256	121.1	0.9088	0.9194	0.9281	0.9356	0.9473
260	123.3	0.9070	0.9177	0.9265	0.9342	0.9406
264	126.7	0.9040	0.9160	0.9251	0.9326	0.9394
268	125.6	0.9050	0.9160	0.9251	0.9326	0.9450
272	129.7	0.9040	0.9151	0.9243	0.9321	0.9388
276	128.7	0.9021	0.9134	0.9228	0.9308	0.9375
280	131.1	0.9002	0.9117	0.9213	0.9294	0.9363
284	132.2	0.8992	0.9108	0.9208	0.9287	0.9357
288	134.4	0.8972	0.9091	0.9190	0.9274	0.9345
292	136.7	0.8953	0.9074	0.9175	0.9260	0.9332
296	136.9	0.8934	0.9057	0.9159	0.9246	0.9320
300	140.0	0.8924	0.9048	0.9152	0.9239	0.9314
304	142.2	0.8904	0.9031	0.9145	0.9226	0.9307
308	144.4	0.8885	0.9014	0.9121	0.9212	0.9289
312	145.6	0.8875	0.9005	0.9114	0.9205	0.9283
316	147.8	0.8866	0.8988	0.9098	0.9192	0.9271
320	150.0	0.8856	0.8971	0.9083	0.9188	0.9263
324	154.4	0.8709	0.8850	0.8983	0.9089	0.9178
328	156.7	0.8699	0.8850	0.8976	0.9082	0.9172
332	159.0	0.8689	0.8845	0.8963	0.9079	0.9164
336	167.8	0.8679	0.8833	0.8960	0.9068	0.9160
340	171.1	0.8669	0.8820	0.8957	0.9075	0.9155
344	173.3	0.8650	0.8785	0.8922	0.9034	0.9129
348	174.4	0.8630	0.8780	0.8914	0.9025	0.9123
352	176.7	0.8620	0.8775	0.8906	0.9016	0.9109
356	176.7	0.8600	0.8763	0.8899	0.9013	0.9110
360	178.9	0.8580	0.8750	0.8883	0.8999	0.9098
364	180.0	0.8570	0.8737	0.8876	0.8992	0.9092
368	182.2	0.8550	0.8720	0.8861	0.8979	0.9079
372	183.3	0.8541	0.8711	0.8853	0.8972	0.9073
376	185.6	0.8521	0.8700	0.8843	0.8961	0.9061
380	187.8	0.8501	0.8676	0.8822	0.8944	0.9048
384	189.9	0.8491	0.8667	0.8814	0.8937	0.9042
388	190.0	0.8481	0.8656	0.8804	0.8926	0.9036
392	191.1	0.8471	0.8650	0.8794	0.8923	0.9030
396	192.2	0.8461	0.8641	0.8791	0.8918	0.9023
400	194.4	0.8441	0.8631	0.8787	0.8914	0.9018
404	196.6	0.8431	0.8620	0.8780	0.8909	0.9015
408	198.7	0.8311	0.8509	0.8674	0.8813	0.8930
412	200.0	0.8301	0.8492	0.8659	0.8809	0.8927
416	212.2	0.8280	0.8482	0.8659	0.8799	0.8918
420	214.4	0.8260	0.8472	0.8659	0.8829	0.8919
424	217.8	0.8230	0.8439	0.8612	0.8757	0.8880
428	220.0	0.8210	0.8430	0.8604	0.8750	0.8870
432	223.3	0.8179	0.8395	0.8573	0.8743	0.8868
436	224.4	0.8169	0.8386	0.8565	0.8715	0.8843
440	226.6	0.8159	0.8377	0.8557	0.8703	0.8836

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### Asphalt Volume Correction Table - 5

CORRECTION FACTORS (to determine volume at 60°F)						
Temperature	Specific Gravity at 60°F	0.800	0.850	0.900	0.950	1.000
316	155.8	0.8758	0.8902	0.9022	0.9123	0.9209
318	158.9	0.8758	0.8902	0.9022	0.9123	0.9283
320	160.0	0.8738	0.8884	0.9006	0.9109	0.9193
324	162.2	0.8728	0.8876	0.8999	0.9102	0.9191
328	164.4	0.8709	0.8856	0.8983	0.9089	0.9178
332	165.6	0.8699	0.8850	0.8976	0.9082	0.9172
336	167.8	0.8689	0.8833	0.8960	0.9068	0.9160
340	171.1	0.8669	0.8815	0.8945	0.9054	0.9147
344	173.3	0.8650	0.8795	0.8922	0.9034	0.9139
348	174.4	0.8630	0.8780	0.8914	0.9025	0.9123
352	176.7	0.8620	0.8770	0.8906	0.9016	0.9119
356	176.7	0.8600	0.8763	0.8899	0.9013	0.9110
360	178.9	0.8580	0.8746	0.8883	0.8999	0.9098
364	180.0	0.8570	0.8737	0.8876	0.8992	0.9092
368	182.2	0.8550	0.8720	0.8861	0.8979	0.9079
372	183.3	0.8541	0.8711	0.8853	0.8972	0.9073
376	185.6	0.8521	0.8699	0.8837	0.8955	0.9061
380	187.8	0.8501	0.8676	0.8822	0.8944	0.9048
384	189.9	0.8491	0.8667	0.8814	0.8937	0.9042
388	190.0	0.8481	0.8656	0.8804	0.8926	0.9036
392	191.1	0.8471	0.8650	0.8794	0.8923	0.9030
396	192.2	0.8461	0.8641	0.8791	0.8918	0.9023
400	194.4	0.8441	0.8631	0.8787	0.8903	0.9011
404	196.6	0.8431	0.8620	0.8780	0.8899	0.9008
408	198.7	0.8311	0.8509	0.8674	0.8813	0.8930
412	210.0	0.8301	0.8492	0.8659	0.8809	0.8927
416	212.2	0.8280	0.8482	0.8659	0.8799	0.8918
420	214.4	0.8260	0.8465	0.8635	0.8777	0.8891
424	217.8	0.8230	0.8439	0.8612	0.8757	0.8880
428	220.0	0.8210	0.8430	0.8604	0.8750	0.8870
432	223.3	0.8179	0.8395	0.8573	0.8722	0.8849
436	224.4	0.8169	0.8386	0.8565	0.8715	0.8843
440	226.6	0.8159	0.8377	0.8557	0.8703	0.8836

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### Asphalt Volume Correction Table - 6

CORRECTION FACTORS (to determine volumes at 60°F)						
Temperature	Specific Gravity at 60°F	0.800	0.850	0.900	0.950	1.000
396	201.1	0.8381	0.8571	0.8729	0.8861	0.8974
398	203.3	0.8361	0.8553	0.8713	0.8847	0.8961
400	205.5	0.8341	0.8530	0.8696	0.8833	0.8949
402	206.7	0.8341	0.8536	0.8696	0.8833	0.8948
404	206.7	0.8331	0.8527	0.8690	0.8827	0.8943
408	208.9	0.8311	0.8517	0.8687	0.8820	0.8933
412	211.1	0.8301	0.8507	0.8674	0.8813	0.8923
416	212.2	0.8280	0.8483	0.8651	0.8792	0.8911
420	214.4	0.8260	0.8465	0.8635	0.8777	0.8891
424	217.8	0.8230	0.8439	0.8612	0.8757	0.8880
428	220.0	0.8210	0.8430	0.8604	0.8750	0.8870
432	223.3	0.8179	0.8395	0.8573	0.8722	0.8849
436	224.4	0.8169	0.8386	0.8565	0.8715	0.8843
440	226.6	0.8159	0.8377	0.8557	0.8703	0.8836

The following formulas are used to calculate the correction factors in the table above.

$$\text{Volume}_{\text{Corrected}} = \text{Volume}_{\text{Measured}} * \frac{1}{\left[ \frac{p_1^2 - p_2^2}{2 * p_1 * p_2} + 1 \right]}$$

Where  $p_1$  = Specific Gravity @ 60° F

And  $p_2$  = Specific Gravity @ Temp. Measured in °F

$$= \sqrt{p_1^2 - [0.0061 * (\text{Temp. Measured in } ^\circ\text{F} - 60^\circ\text{F})]}$$

Reference: Perry's Chemical Engineers' Handbook, 6th edition, 1984,

McGraw-Hill, R660.28P or 660.2

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### Temperature/Volume Example

- Asphalt Sp. Gr. = .950 @ 60°F; asphalt volume @ 200°F = 2,000 gallons; determine the asphalt volume @ 60°F

➤ Solution:

C.F. = .9526 (from asphalt conversion table)

$$2,000 \times .9526 = 1,905 \text{ gallons @} 60^{\circ}\text{F}$$

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### Correction Factor Interpolations

- If the specific gravity equals 0.985 at 60°F and the volume measured equals 9,000 gal at 180 °F, read the table at 180°F and interpolate between 0.9593 and 0.9633 (from the 0.950 column and the 1.000 column) as follows:

$$0.9593 + \left( \frac{0.9633 - 0.9593}{1.000 - 0.950} \right) \times (0.985 - 0.95) = 0.9593 + 0.0028 = 0.9621$$

- Therefore, the corrected volume at 60 equals 9,000 gal x 0.9621 equals 8659 gal.

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### Partially Filled Tank

To determine partially filled volume:

- Measure asphalt depth
- Calculate % of depth filled
- Enter table and select % of volume filled
- Calculate volume of asphalt

Vol. = % of vol. filled x capacity

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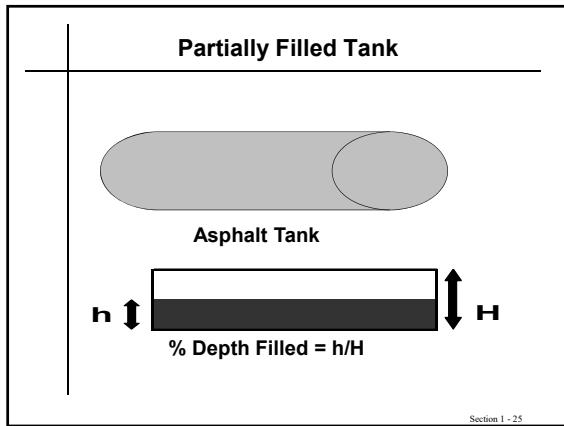
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% DEPTH FILLED	% OF CAPACITY						
0	1.27	26	20.66	51	51.28	76	81.54
1	0.48	27	21.78	52	52.54	77	82.69
2	0.28	28	22.88	53	53.62	78	83.83
3	0.14	29	24.07	54	55.09	79	84.73
4	0.07	30	25.23	55	56.36	80	85.76
5	0.45	31	26.41	56	57.62	81	86.77
6	3.03	32	27.57	57	58.78	82	87.83
7	3.75	33	28.78	58	60.41	83	88.73
8	3.75	34	29.98	59	61.40	84	89.67
9	5.20	35	31.19	60	62.65	85	90.62
10	5.98	36	32.41	61	63.89	86	91.49
11	7.01	37	33.65	62	65.13	87	92.36
12	7.64	38	34.87	63	66.36	88	93.20
13	8.51	39	36.07	64	67.59	89	94.04
14	9.41	40	37.35	65	68.81	90	94.80
15	10.33	41	38.60	66	70.02	91	95.54
16	11.27	42	39.83	67	71.22	92	96.27
17	12.24	43	41.12	68	72.41	93	96.92
18	13.23	44	42.38	69	73.59	94	97.55
19	24.44	45	43.64	70	74.77	95	98.13
20	15.37	46	44.81	71	75.93	96	98.66
21	16.31	47	46.18	72	77.08	97	99.13
22	17.38	48	47.46	73	78.22	98	99.52
23	18.46	49	48.73	74	79.34	99	99.83
24	19.56	50	50.00	75	80.49		

